Fast Whole-Engine Stirling Analysis





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Thermal Energy Conversion Branch

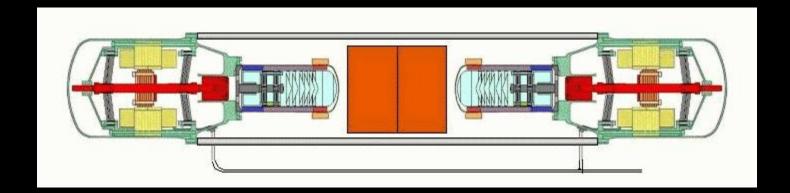
August 16, 2005





Dual Opposed Stirling Convertors

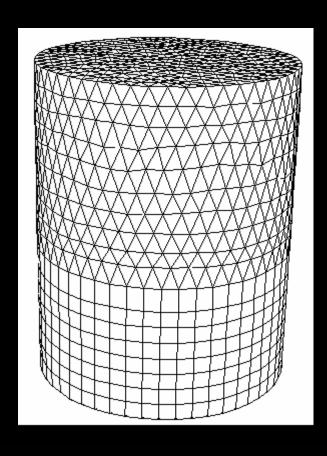
High Efficiency, Low Mass Space Power

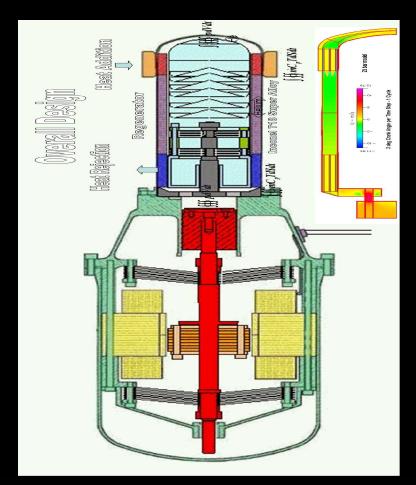






Simulate Engine Only











Operating Conditions

Hot-End Temperature, K 923

Cold-End Temperature, K 353

Ambient Temperature, K 293

Frequency, Hz 80

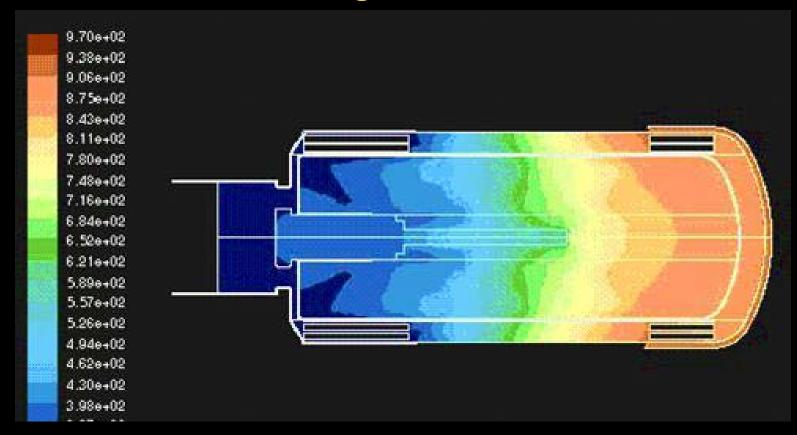
Mean Pressure, Pa 2.429E+6

Power Piston Amplitude, mm 6.0e-3





Whole-Engine Simulation









Comparison with Sage 1D Results

	Axisymmetric	Sage 1D	Sage 1D	
	Simulation	Ambient	No Ambient	
PV Power, W	79.65	68.77	70.14	
Heat In, W	247.315	260.94	193.8	
Heat Out, W	168.313	191.9	123.7	
PV Efficiency	.322	.264	.362	
Pressure Ratio	1.209	1.187	1.187	
Regen. ∆P., Pa	10466.3	15888	15790	
Heater P, Pa	682	194	192	
Cooler P, Pa	896	316	315	
Pressure Amp., Pa	225269	203100	203200	
Mean Pressure, Pa	2429130	2378000	2378000	



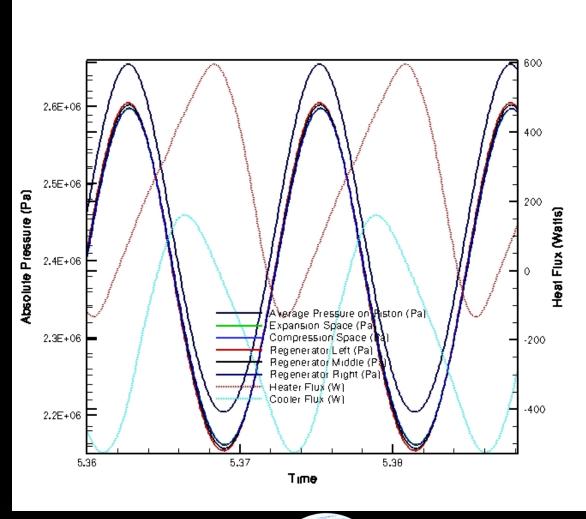
Comparison with Experiment

	Thot C	Tcold C	Freq. Hz	Qin W	PV W	Qout W
TDC #13	646.0	80- 92.4	81.4	242.1	78.2	163.9
TDC #14	646.5	80- 94.4	81.4	250.4	79.6	170.8
Simulation	650.0	80	80	247.3	79.7	168.3
%Err-AVE	100.6	?	98.2	100.4	100.9	100.6





Pressure and Heat Transfer over Cycle

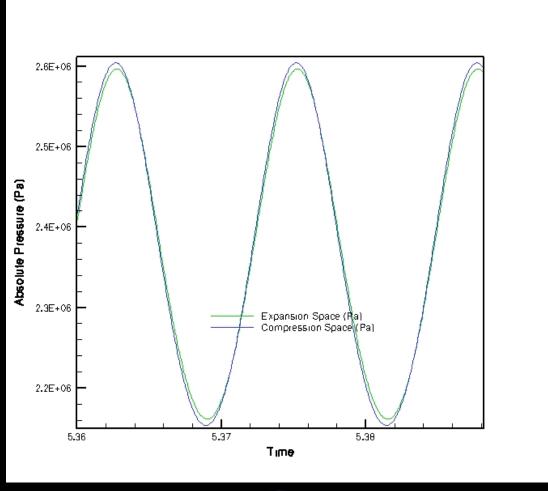








Expansion and Compression Pressure

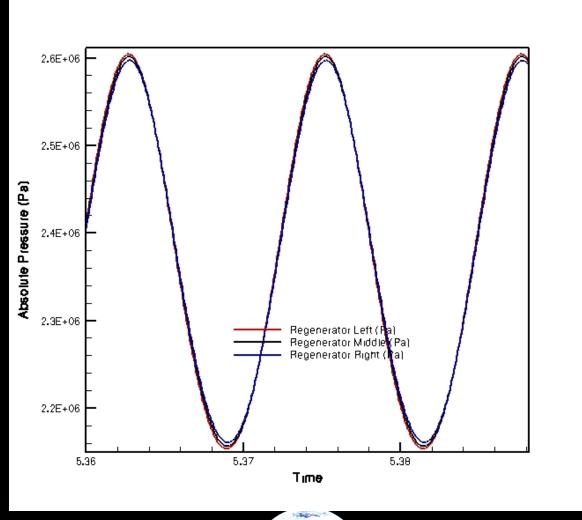








Regenerator Pressure Drop







Solved Whole-Engine On 32 Processor Cluster







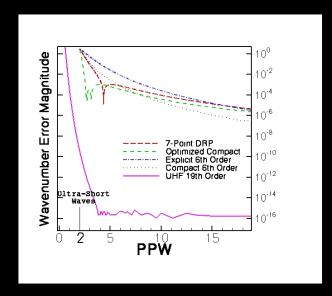


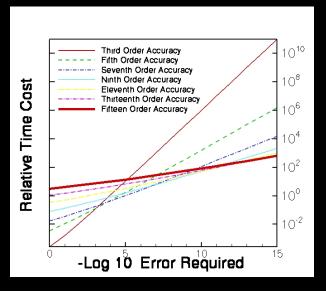




Multidimensional Analysis Tools

- Modified CAST, CFD-ACE, Fluent, STAR-HPC, CFX/ANSYS, others ...
- All low order SIMPLE/PISO based
- New high-order codes being developed









Multidimensionally Enabled Capabilities

- Structural, thermal, fluid, electromagnetics, and coupled physics.
- 1 hour per cycle axisymmetric simulation
- Seal & appendix gap phenomena
- HX end effects
- Effect of vortices in expansion & compression
- Flexure temperatures for reliability analysis
- Effects of slight geometrical variations

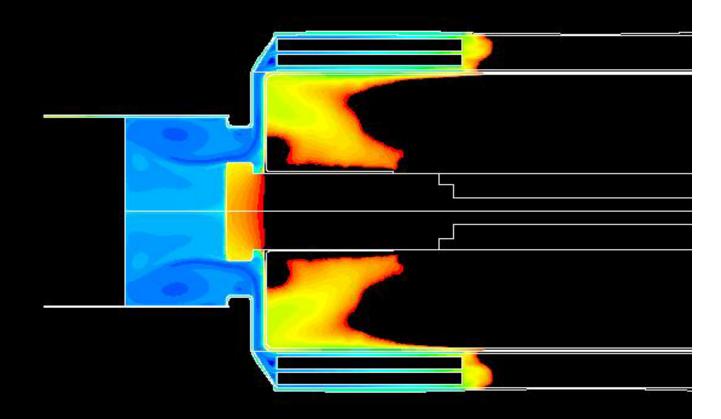




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Cool End Heating

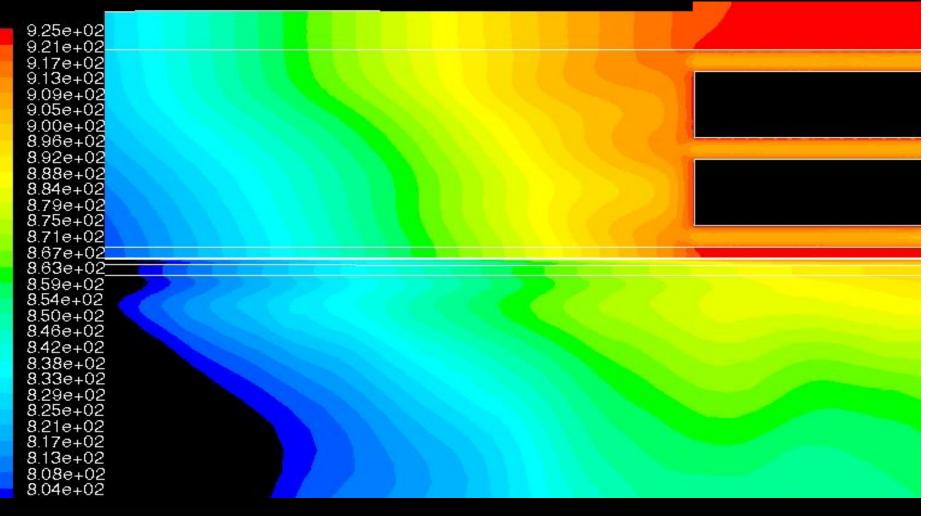
3.75e+02 3.74e+02 3.73e+02 3.71e+02 3.70e+02 3.69e+02 3.68e+02 3.67e+02 3.66e+02 3.64e+02 3.63e+02 3.62e+02 3.61e+02 3.60e+02 3.58e+02 3.57e+02 3.56e+02 3.55e+02 3.54e+02 3.53e+02 3.51e+02 3.50e+02 3.49e+02 3.48e+02 3.47e+02 3.45e+02 3.44e+02 3.43e+02 3.42e+02 3.41e+02







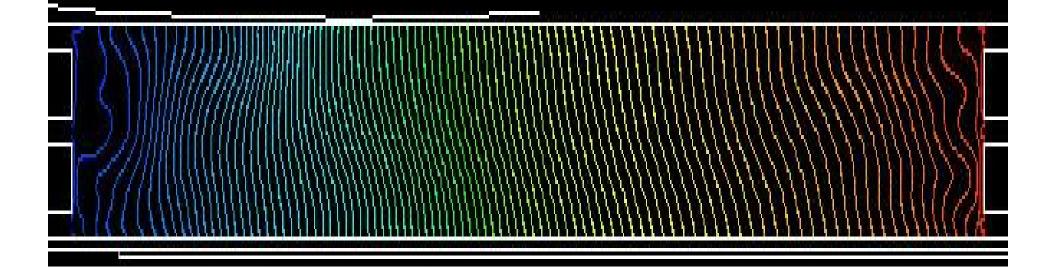
Radial Heat Transfer Effects







Radial Heat Transfer Effects

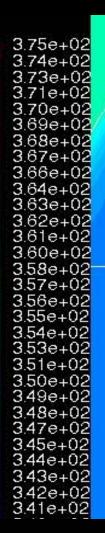














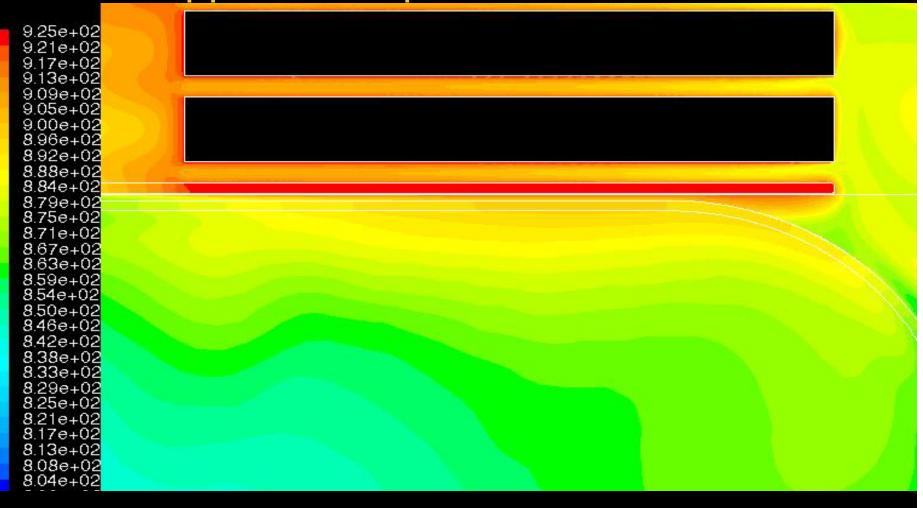
Displacer Seal Close-up







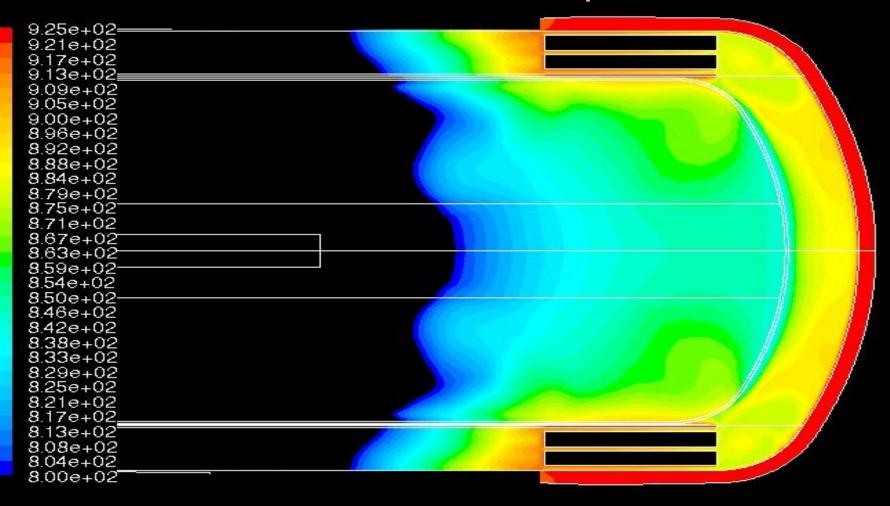
Appendix Gap Shuttle Losses







Effects of Vortices in Expansion







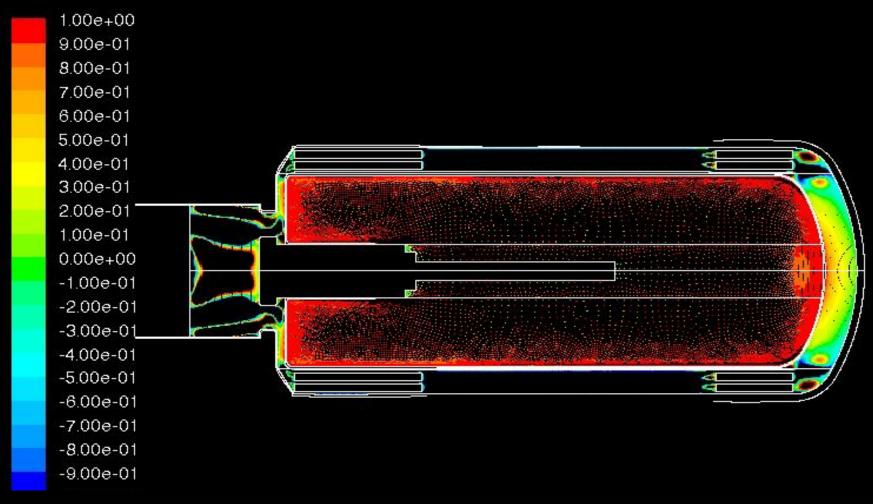
Simulation Approach

- Whole-engine for physical consistency
- REV Regenerator Modeling
- Grid Layering, Smoothness, and Quality
- Conjugate heat transfer method adjustment
- High-speed Low Cost Parallel Cluster
- Lot's of debugging....





Dangers of Component Modeling: Axially Oscillating Boundaries







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Radially Oscillating Boundaries

9.00e-01

1.00e+00

8.00e-01

7.00e-01

6.00e-01

5.00e-01

4.00e-01

3.00e-01

2.00e-01

1.00e-01

0.00e+00

-1.00e-01

-2.00e-01

-3.00e-01

-4.00e-01

-4.00e-0

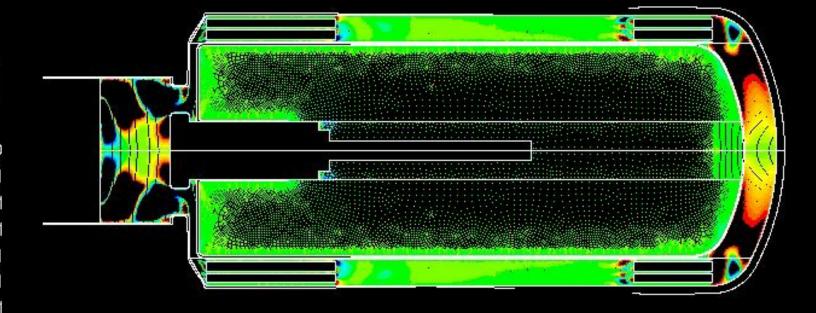
-5.00e-01

-6.00e-01

-7.00e-01

-8.00e-01

-9.00e-01

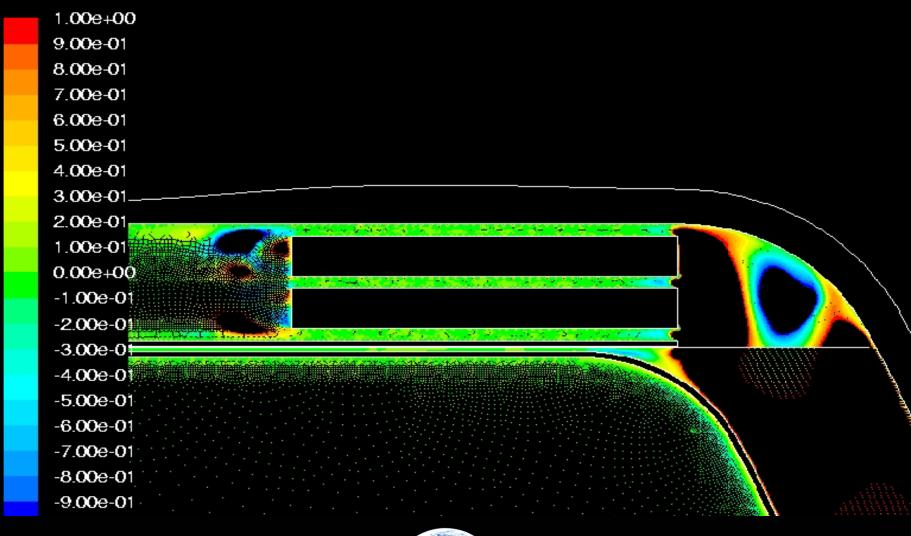








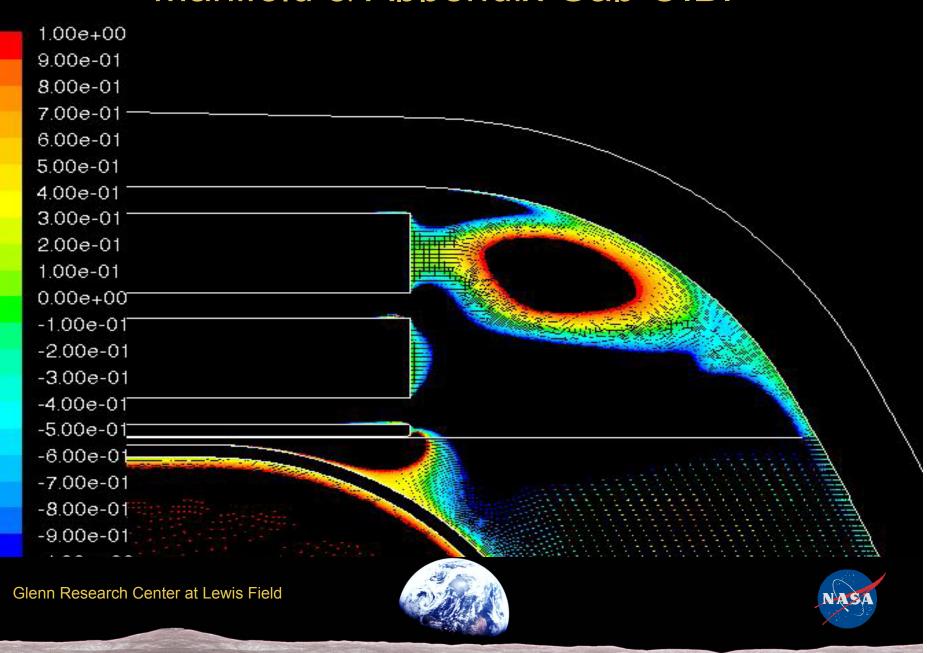
Heat Exchanger Oscillating Boundary



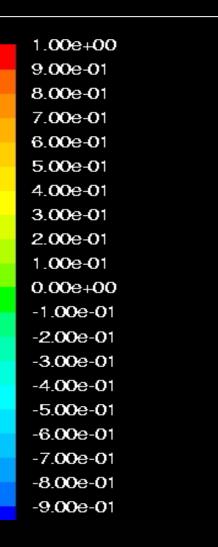


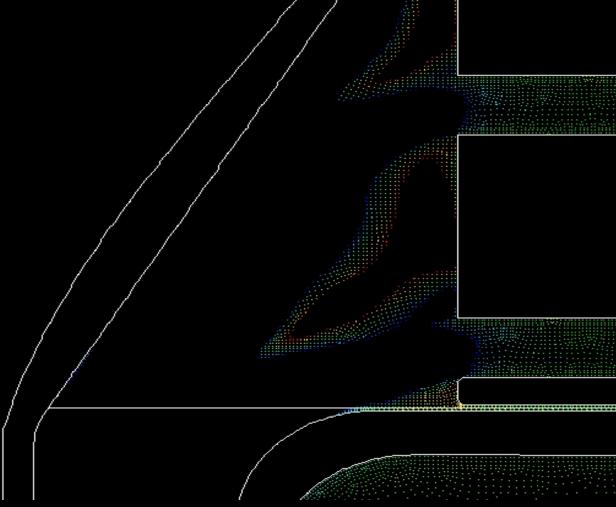


Manifold & Appendix Gap O.B.



Cooler Manifold O.B.

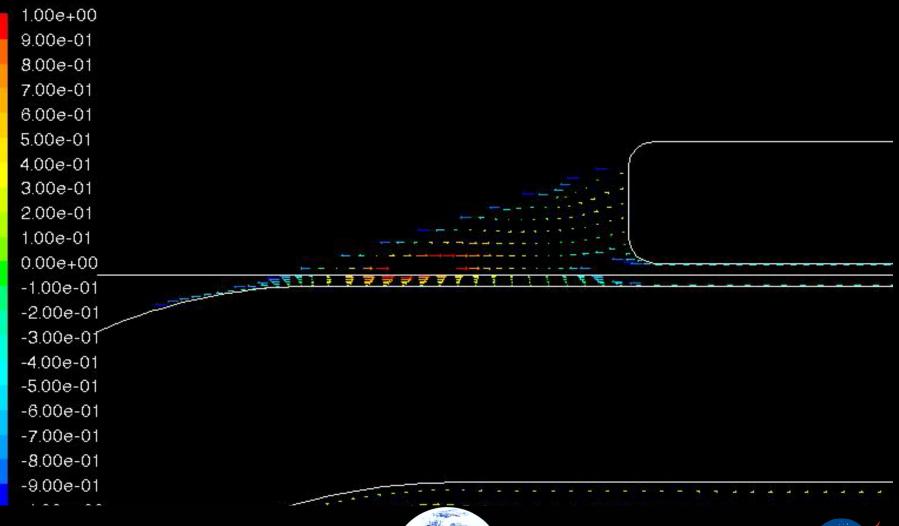






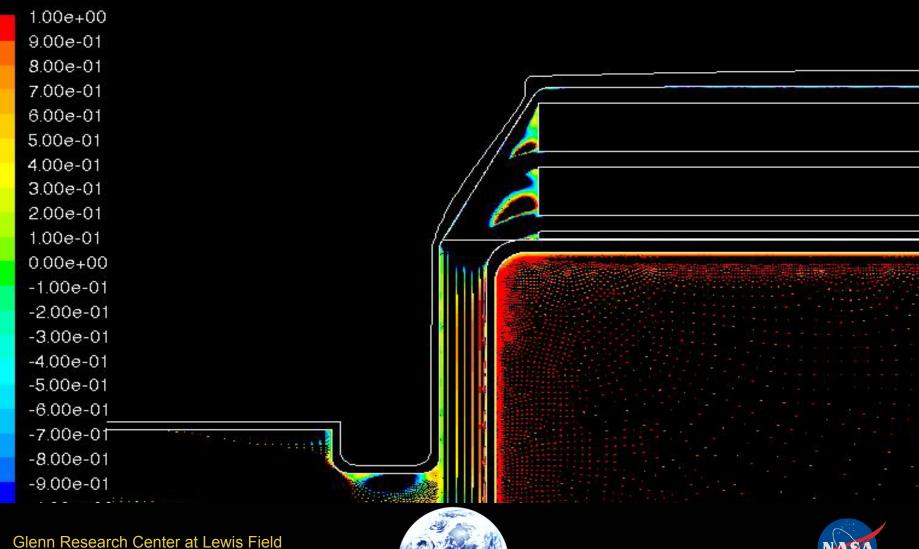


Seal Region O.B.





Compression Manifold O.B.





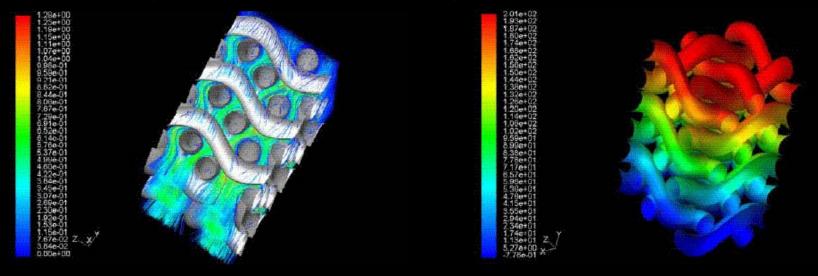
Regenerator Modeling

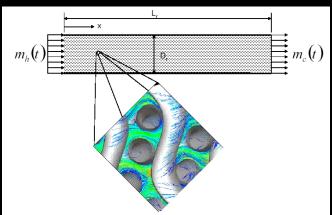
- Geometrical Shapes Affect Complexity
- High Efficiency Regenerators Permit Thermal-Equilibrium Assumption/Usage
- Add source terms to governing equations
- Darcy-Forcheimer equation is used on momentum, Coefficients from experiment
- Single Energy equation (fluid/solid averaged) with averaged conductivity and energy





Regenerator Modeling in More Detail Later

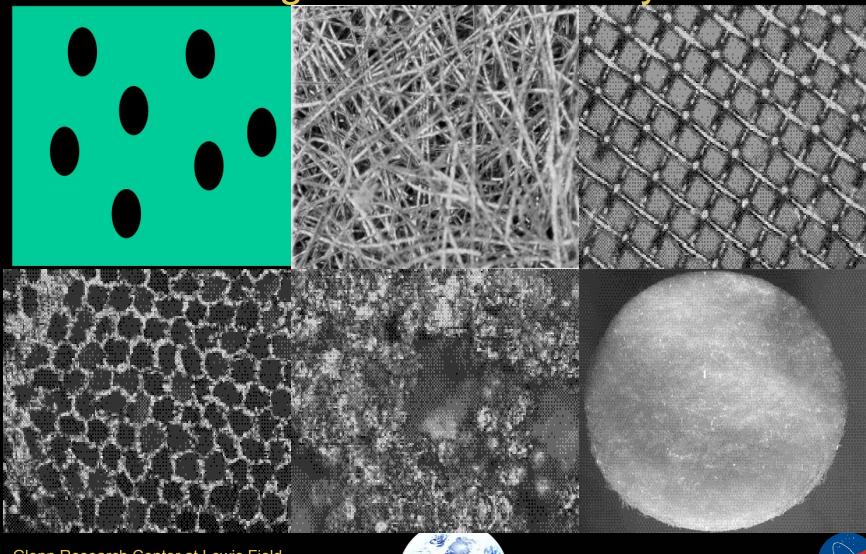








Regenerator Geometry







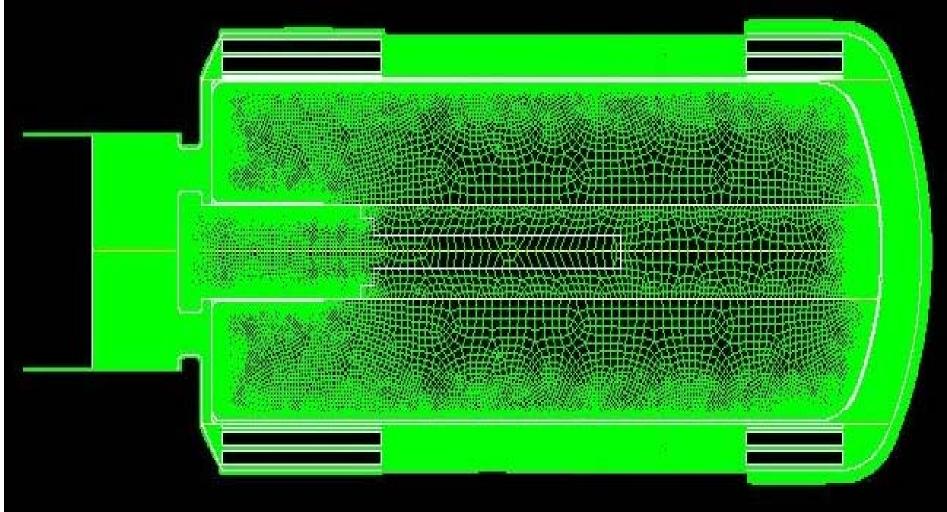
Gridding Approach

- Scale geometry to compensate for 32-bit
- Avoid tetrahedrals, use unstructured quads
- Match cell sizes across sliding regions
- Smoothly expand/shrink cell sizes throughout
- Use layering, avoid adaption/remeshing
- Utilize moving and double-sided boundary layers
- Include as much geometry as practical
- Clean up geometry in CAD, avoid virtual geometry
- Over-converge the steady solution to improve grid





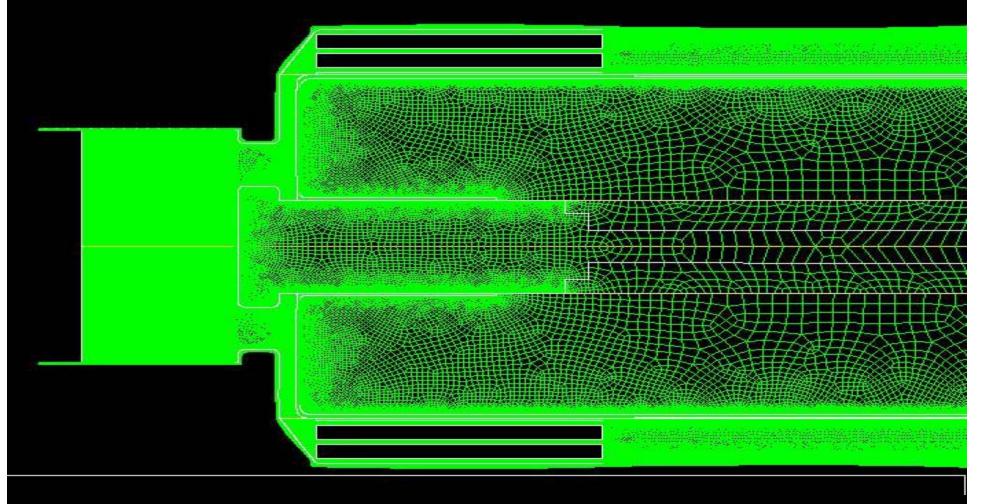
Whole Engine (700K cells)







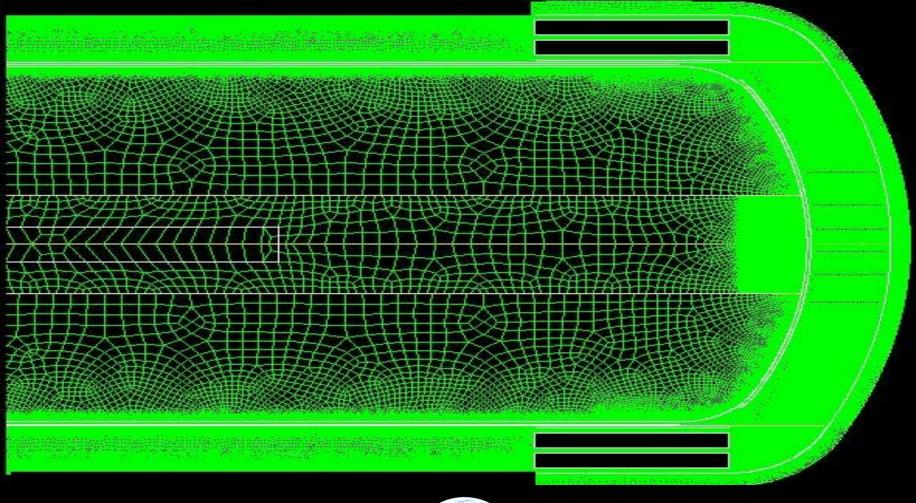
Left Half Grid





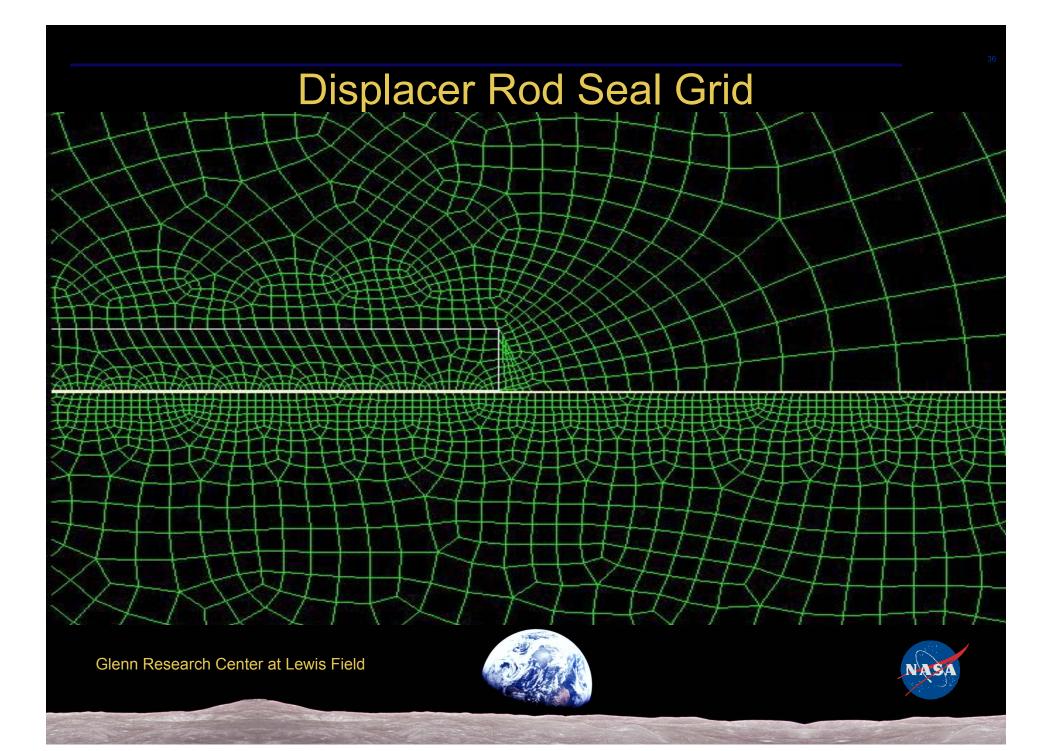


Right Half Grid

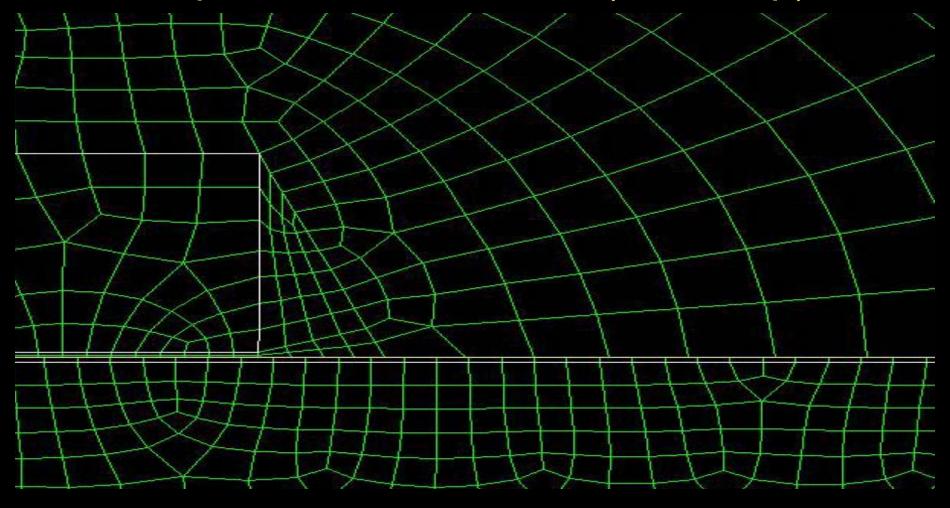








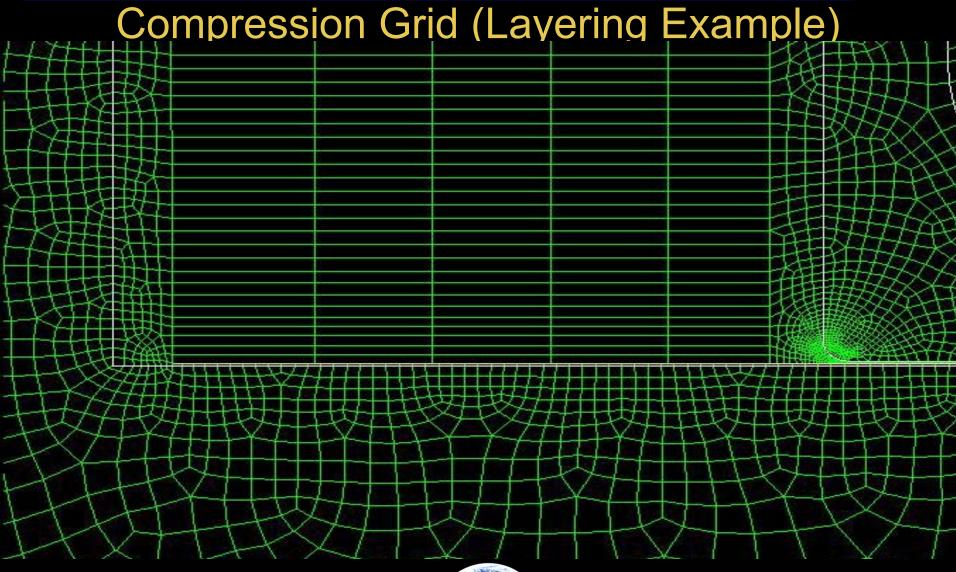
Displacer Rod Seal Grid (Close-Up)





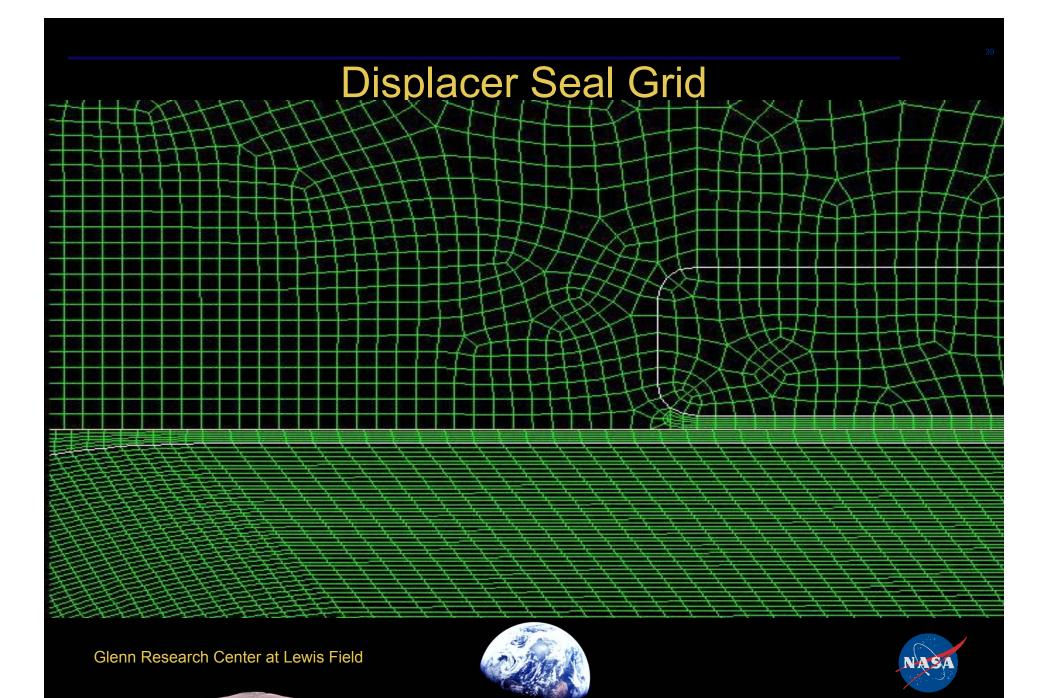


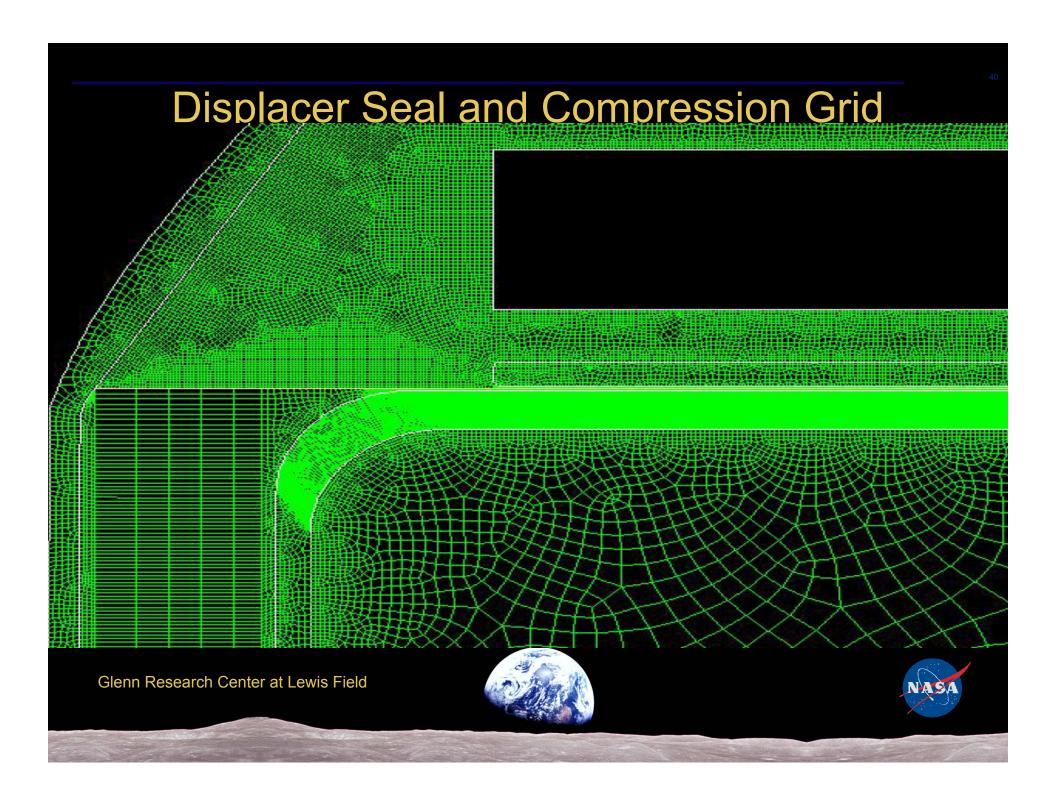


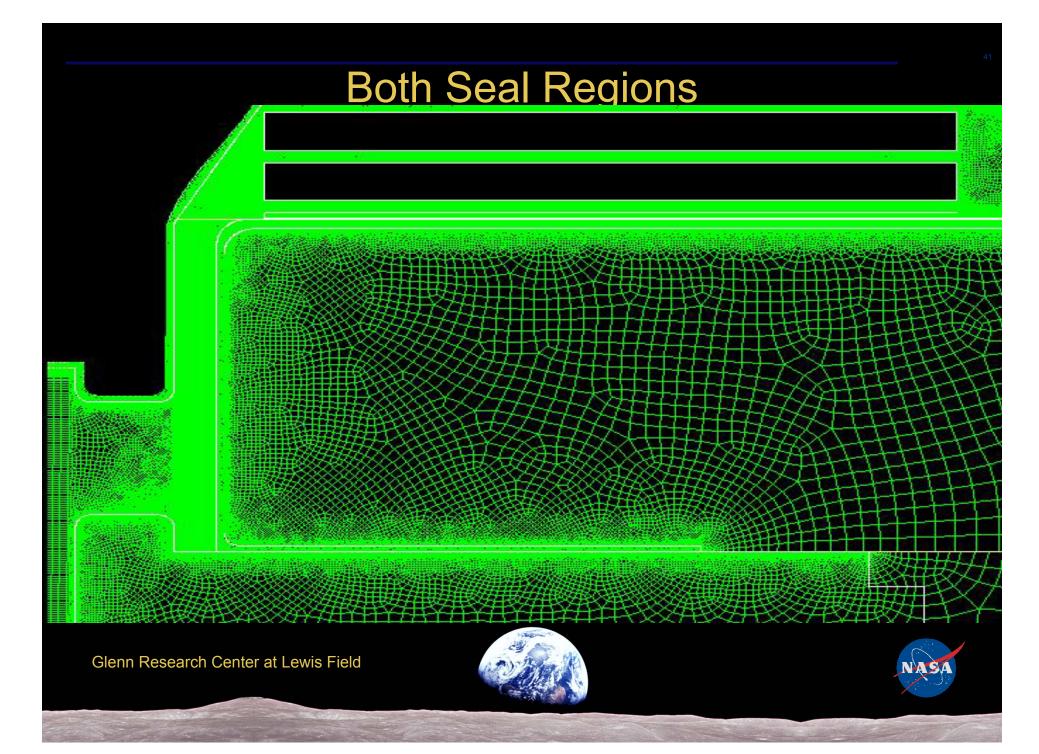


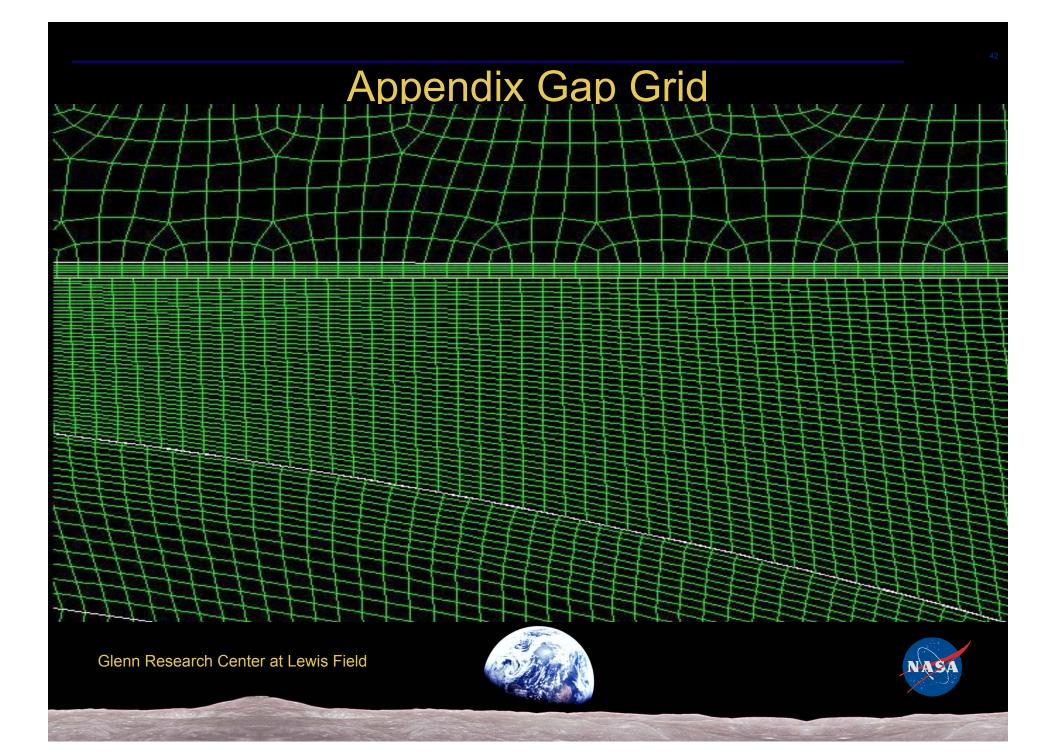




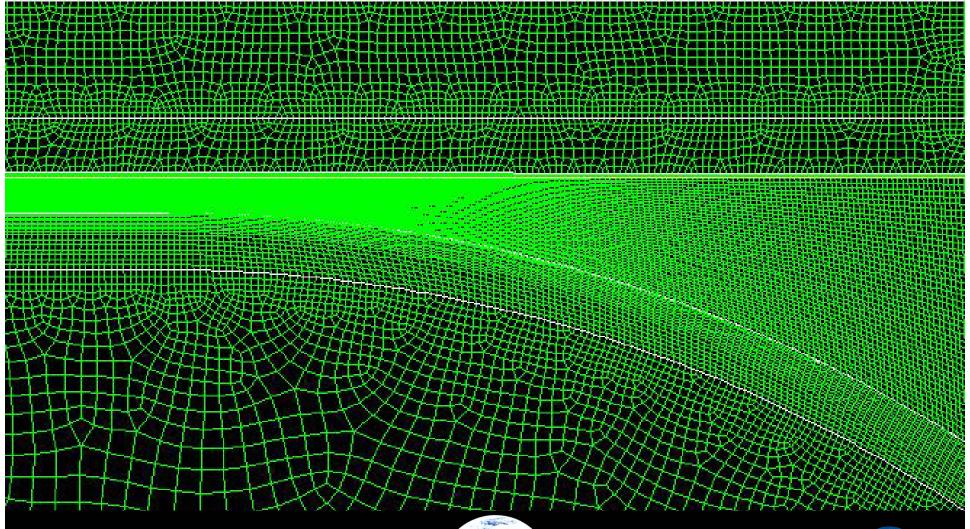






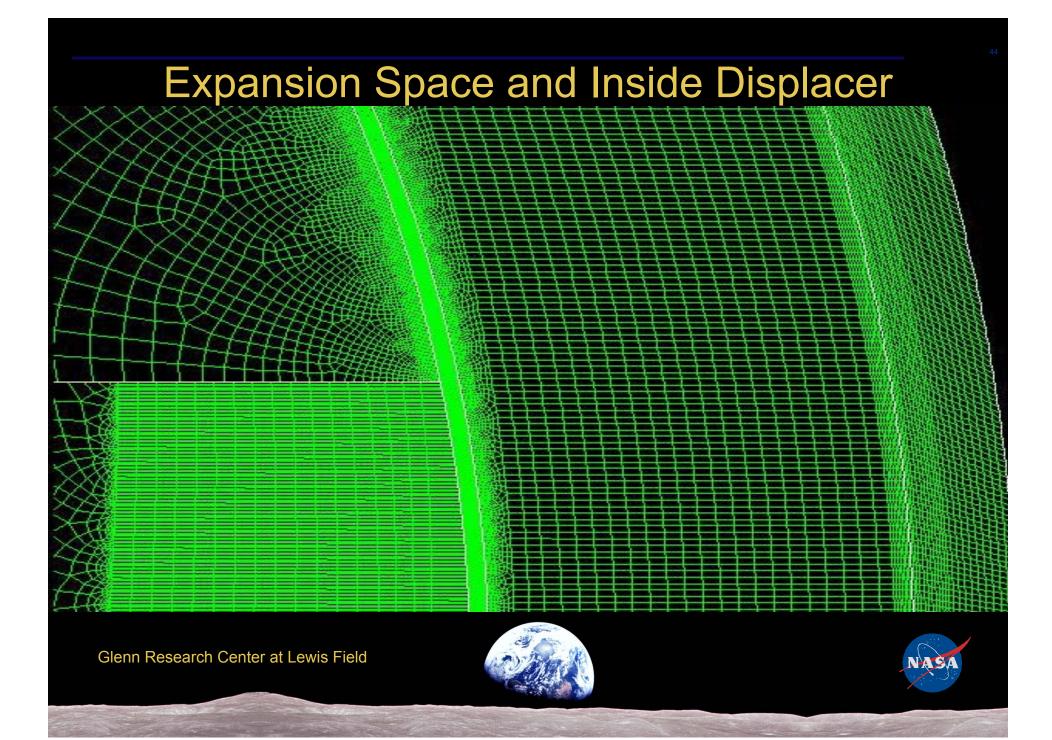




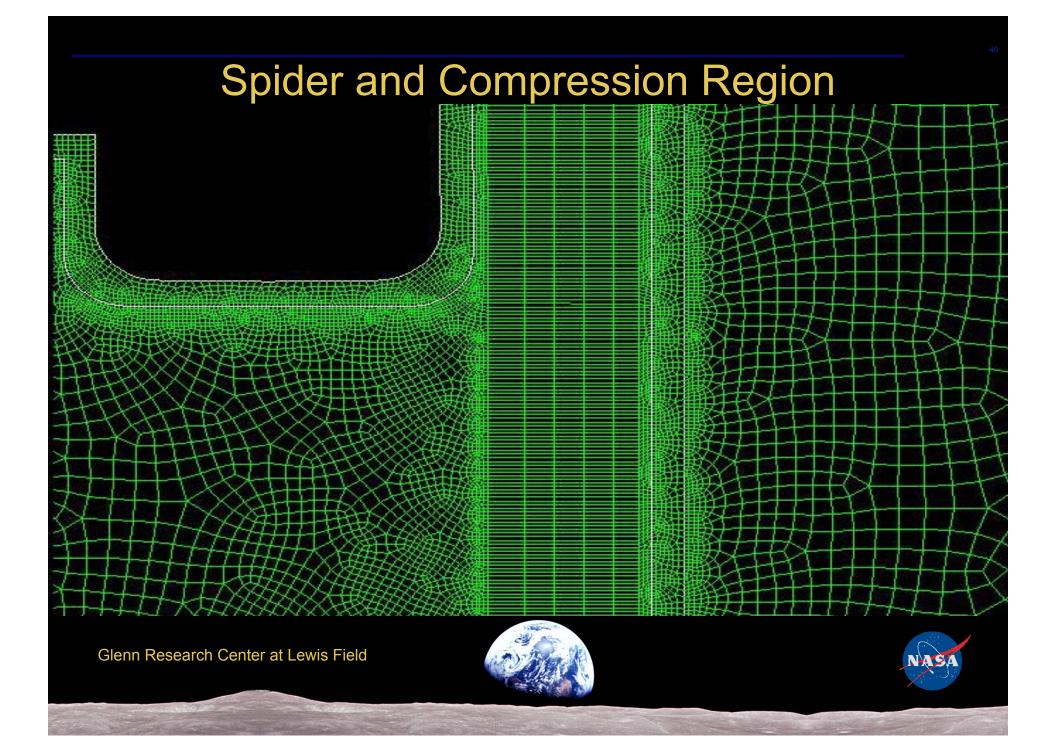




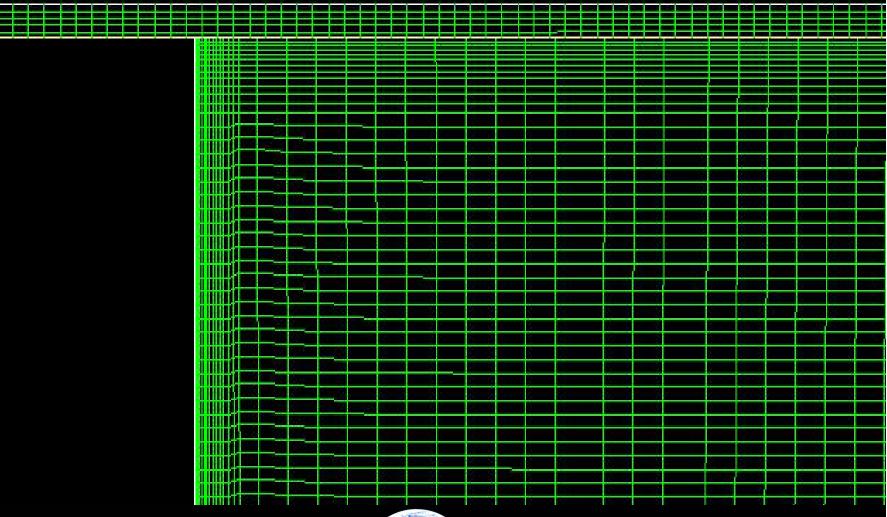




Inside Displacer and Wall Glenn Research Center at Lewis Field



Piston Region







Conjugate Heat Transfer Strategy

- Utilize coupled solver in double precision
- Maximize energy underrelaxation factor
- Double-sided boundary layers
- Turn off secondary temperature gradients
- Emphasize the coarse multigrid to avoid roundoff error
- Utilize explicit underrelaxation of temperature
- Maintain small time-steps (160/cycle)
- Go to higher space and time accuracy when possible







Higher Solution Speeds Achievable

- •Infiniband/High Capacity Switch
- •260 processors in a single 7 foot tower
- •Higher-Order Techniques
- Quad/Octa Opteron Processors
- •256 bit computing

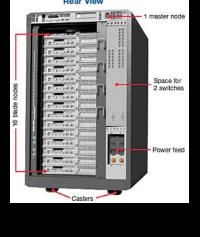














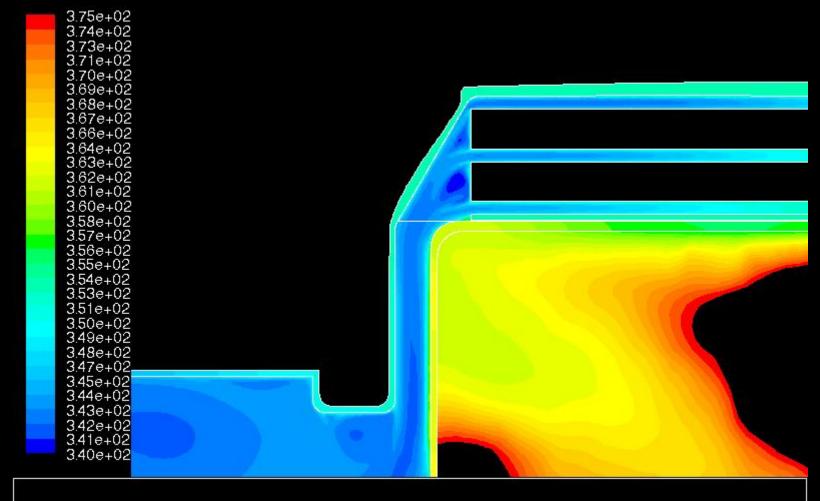
Conclusions

- First U.S. fully converged axisymmetric simulation of actual Stirling engine
- Comparison with experiment shows less than 1% error on power and efficiency
- More testing required to confirm
- Extending to three-dimensions for full part testing and integration





Cool End Heating

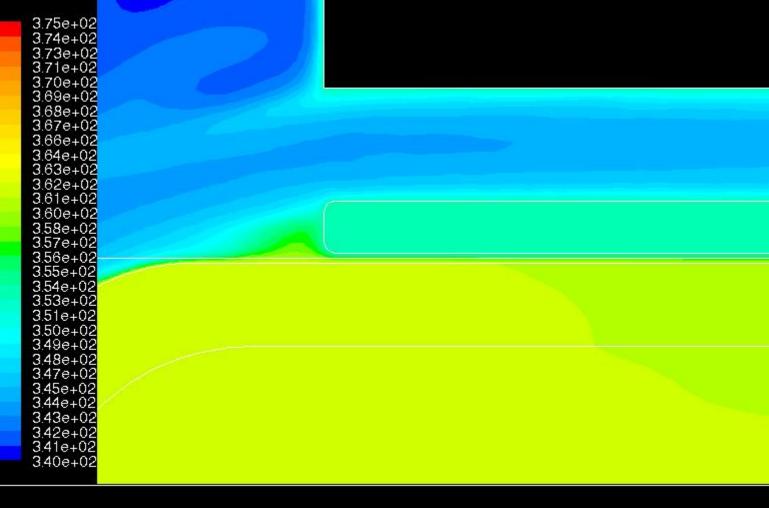


Contours of Static Temperature (k) (Time=5.1547e+00)









Contours of Static Temperature (k) (Time=5.1547e+00)







Displacer Seal Leakage

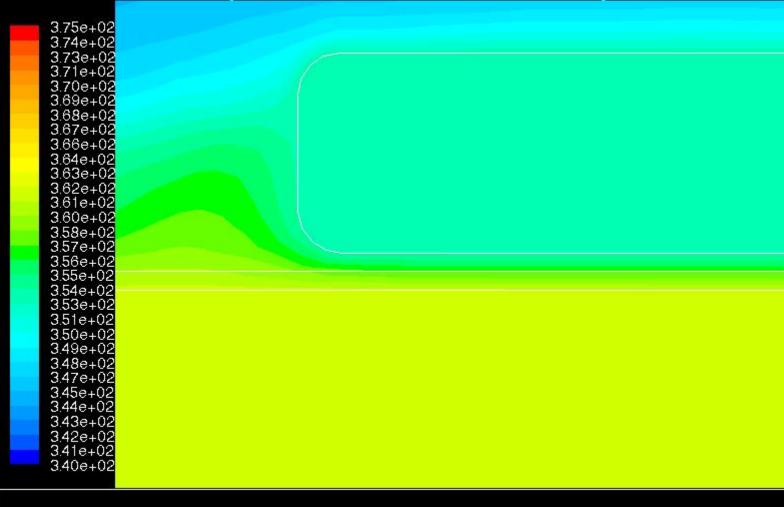


Contours of Static Temperature (k) (Time=5.1547e+00)





Displacer Seal Close-up

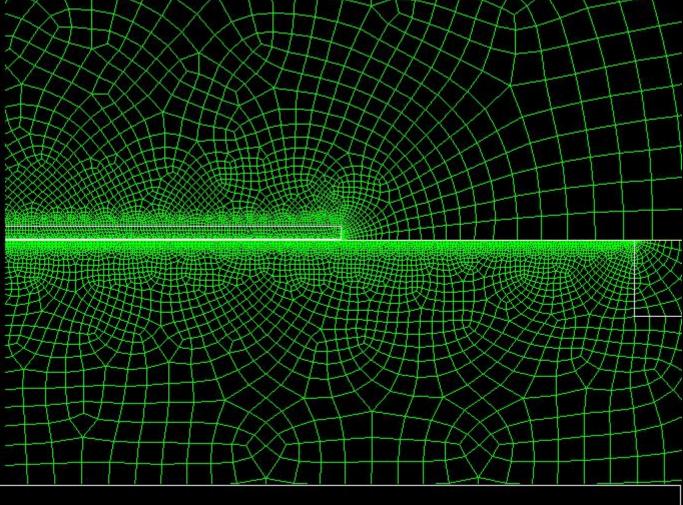


Contours of Static Temperature (k) (Time=5.1547e+00)





Displacer Rod Seal Grid



Grid (Time=5.1547e+00)



